Publications of the Institute of Geophysics, Polish Academy of Sciences

Geophysical Data Bases, Processing and Instrumentation

vol. 434 (E-11), 2021, pp. 101-103

DOI: 10.25171/InstGeoph_PAS_Publs-2021-030

Webinar on Experimental Methods and Laboratory Instrumentation in Hydraulics, 13-15 April 2021

Experimental Test Bench for Performance-Assessment of Large Submersible and Dry-Action Pumps Used in Waterways

Joris HARDY^{1,∞}, Pierre DEWALLEF¹, Sébastien ERPICUM¹, Michel PIROTTON¹,
Darren PARKINSON², Nigel TAYLOR², Chris BARNET², Paula TREACY³,
Olivier THOMÉ¹, Pierre ARCHAMBEAU¹, and Benjamin DEWALS¹

¹Université de Liège, School of Engineering, Liège, Belgium

²Canal & River Trust (CRT), United Kingdom

³Waterways Ireland (WI), Ireland

⊠ joris.hardy@uliege.be

Abstract

Pumping in waterways, particularly in artificial canals, is energy-intensive, costly and may be responsible for the emission of large quantities of CO₂. Innovative pumping technologies have the potential to reduce energy consumption; but their performance needs to be thoroughly assessed. This communication presents the design, sizing and construction of an experimental test bench for evaluating the performance of large submersible and dry-action centrifugal pumps typically used in waterways. It enables testing prototype-scale pumps and was designed in close collaboration with stakeholders such as canal operators. This experimental facility is challenging on many aspects given its size, as well as requirements for power supply and for measurement of system efficiency.

Keywords: experimental test bench, waterways, pumps, stainless steel pipe design, flow instrumentation.

1. DESIGN AND SIZING

The overall objective of the test bench is to enable monitoring the efficiency of submersible and dry-action centrifugal pumps under a broad range of operating conditions. The primary goal

^{© 2021} The Author(s). Published by the Institute of Geophysics, Polish Academy of Sciences. This is an open access publication under the CC BY license 4.0.

102 J. HARDY et al.

being the assessment of pumps typically used for lifting water in artificial waterways, the capacity requirements for the test bench were defined in close collaboration with stakeholders, mostly canal operators. This lead to the following specifications: pressure up to 10 bars, flow rate up to 0.3 m³/s, power supply up to 300 kW and pumps of up to 2 tons in weight (Table 1). Given these specifications, various aspects of the test bench were designed and sized: layout of stainless steel pipes, pipe diameters, water supply system, regulating valve, energy dissipation system, power electronic boxes with safety and emergency systems, pressure measurement devices and release of entrapped air, among others. A closed-loop system was selected. The overall layout is represented in the CAD model shown in Fig. 1. The positioning of dry-action pumps to be tested is sketched on the right side of the figure, while submersible pumps to be tested shall be installed inside the large tank (visible on the left of the figure).

Table 1
Main characteristics of the test bench

Tank characteristics		Pump characteristics		Test bench characteristics	
Weight	3.5 T	Weight max	2 T	Sensors	10+
Capacity	30 m ³	Power max.	300 kW	Area	8 m × 10 m
Diameter	3 m	Flow rate max.	300 1/s	Piping weight	2 T
Height	4.5 m	Pressure max.	10 bar	Height max.	4.5 m

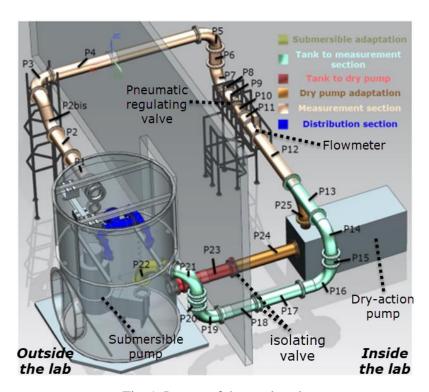


Fig. 1. Layout of the test bench.

The measurement system includes a flowmeter, a regulating valve (to adjust the head), pressure transducers as well as a power analyser and NI data logger. The main pipes have a diameter DN350, allowing friction losses to remain relatively low and ensuring that the diameter of the pump outlet is smaller than the pipe diameter. Sufficiently long straight pipe sections are placed

at the inlet of the flowmeter as well as for the suction pipe of dry-action pumps, to ensure uniform velocity distribution and equalised pressure on the considered section as this helps avoiding swirl conditions.

The diameter and the height of the main tank were determined to prevent swirl conditions at the inlet of the submersible pumps (Sulzer-Pumpen 2010). Given the resulting dimensions (3 m in diameter and 4.5 m in height), the main tank was not available off-the-shelf; but it was manufactured on purpose for the test bench. It is made of stainless steel and its sizing accounts for a variety of constrains, including mechanical strength (finite element simulations were performed to size the curved door and lid), manufacturing process, pump installation procedure and test operations. The door is curved to withstand the inside pressure when the tank is filled with water. The stainless steel sheets are all minimum 6 mm thick. An energy dissipation system, made of several distribution pipes (in dark blue in Fig. 1), is installed at the inlet of the tank to further contribute to avoiding swirl conditions close to the inlet of submersible pumps. A regulating valve is used to adjust the head losses in the hydraulic loop by varying the valve opening angle (between 30° and 70°). Given the specifications on the operation range of the pumps to be tested, a butterfly valve of diameter DN200 was selected.

2. OPERATION

Once a pump is installed, the operating procedure is the same for both submersible and dryaction pumps. The regulating valve and the rotation speed of the pump are electronically steered to browse a range of operating points. The pump is started at its nominal rotating speed, with the lowest opening angle of the regulating valve (30°). While the measurements in the bench are continuously recorded at a high frequency, the opening angle is increased by steps of 10°, up to the maximum flow rate of the pump or the valve maximum opening angle is reached. Then, the operation is repeated in reversed order, by decreasing the valve opening angle by steps of 10°. Next, the pump rotating speed is decreased by a predefined step and the whole operation is repeated again. This enables characterizing steady operating points of the pump for a representative range of heads and rotational several speeds. The characteristic curve of the pump can be redrawn with associated performance for nominal and non-nominal operation. Submersible pumps to be tested are placed inside the tank through the door using a fork truck lift machine and the bridge crane installed at the top of the tank while dry-action pumps are placed inside laboratory.

Acknowledgments. This research is partly supported by ERDF funding in the framework of the Interreg NWE project Green WIN. CRT and WI are gratefully acknowledged.

References

Sulzer-Pumpen (2010), Special data for planning centrifugal pump installations. **In:** Sulzer-Pumpen (eds.), *Centrifugal Pump Handbook*, 3rd ed., Elsevier Science, 91–97.

Received 22 March 2021 Accepted 12 April 2021